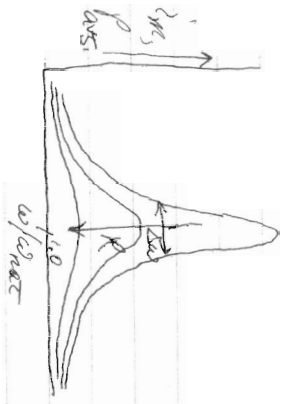


Resonance

The expression $i_{\text{max}} = V_m / \sqrt{R^2 + (\omega L - 1/\omega C)^2}$ gives the condition for max. current (or $i_{\text{max}} = I_{\text{RMS}}$) as

$$\frac{1}{\omega C} = \omega L \Rightarrow \omega_{\text{max}} = \frac{1}{\sqrt{LC}}$$

which is the same as the natural frequency of the LC components.



Peak narrows as R decreases

→ would 0 width if R = 0 (i.e., LC circuit case)

It's useful to define a parameter

$$Q = \frac{i_{\text{max}}}{\Delta i} = \frac{i_{\text{max}}}{R} \quad \text{width when } R = \frac{1}{2} \text{ maximum}$$

①

P 33.29: RLC Circuit

$$\Delta V(t) = V_{\text{max}} \sin(\omega t) \quad \omega$$

Also: $L = 160 \text{ mH}$, $C = 99 \mu\text{F}$, $R = 68 \Omega$

a) I impedance?

$$\begin{aligned} Z &= \sqrt{R^2 + (X_L - X_C)^2} \\ &= \sqrt{68^2 + (100 \cdot 0.16 \text{ H} - \frac{1}{100 \cdot 99 \times 10^{-6} \text{ F}})^2} \\ &= \sqrt{11849 \Omega^2} \\ &= 108.9 \Omega \end{aligned}$$

b) maximum current?

$$\begin{aligned} I_{\text{max}} &= V_{\text{max}} / Z \\ &= 40 \text{ V} / 108.9 \Omega \\ &= \boxed{0.37 \text{ A}} \end{aligned}$$

c) phase?

$$\begin{aligned} \phi &= \tan^{-1} \left(\frac{X_L - X_C}{R} \right) \\ &= \tan^{-1} \left(\frac{100 \cdot 0.16 \text{ H} - \frac{1}{100 \cdot 99 \times 10^{-6} \text{ F}}}{68 \Omega} \right) \\ &= \tan^{-1} (-1.25) \\ &= \boxed{-0.896 \text{ rad}} \end{aligned}$$

So, $i(t) = 0.37 \text{ A} \sin(100t + 0.896 \text{ rad})$

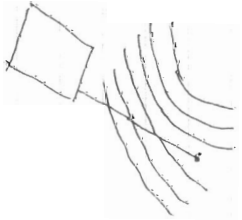
Since $X_C > X_L \rightarrow \phi < 0$ and current leads the voltage

①.5

Radio:

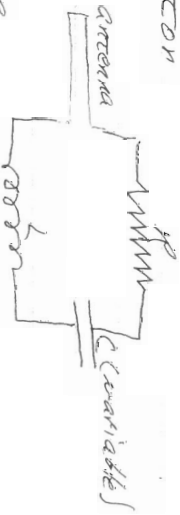
radio waves (oscillating $E + B$ fields)

- when impinge on antenna



- induce emf + current on antenna

Attach to RLC circuit with a variable capacitance



Adjust capacitance C so that ω_{ext} changes.

- when $\omega_{ext} = \omega_{res}$ then induced emf gives maximum current in circuit.

choose R so that have desired Q in narrow range of ω 's (like fm $\approx 10^4$) (88MHz - 108MHz)

- so tuning a radio makes it sensitive to different ω of incoming EM wave

- important to have a narrow filter to distinguish overlapping signals

(2)

P33.38: AM tuning

LC combination used

$$L = 0.2 \text{ mH}$$

$C = \text{variable}$

→ circuit can resonate for range of frequencies from 550kHz to 1650kHz

what is range needed for C ?

$$\omega_{low} = 2\pi f = 2\pi \cdot 550 \text{ kHz} = 3500 \text{ rad/s}$$

$$\omega_{high} = 2\pi f = 2\pi \cdot 1650 \text{ kHz} = 10400 \text{ rad/s}$$

$$\text{Since } \omega_{res} = \frac{1}{\sqrt{LC}} \Rightarrow LC = \frac{1}{\omega_{res}^2}$$

$$C = \frac{1}{L\omega_{res}^2}$$

$$C_{low} = [0.2 \times 10^{-3} \text{ H} \cdot (3500 \text{ rad/s})^2]^{-1}$$

$$= 408 \mu\text{F}$$

$$C_{high} = [0.2 \times 10^{-3} \text{ H} \cdot (10400 \text{ rad/s})^2]^{-1}$$

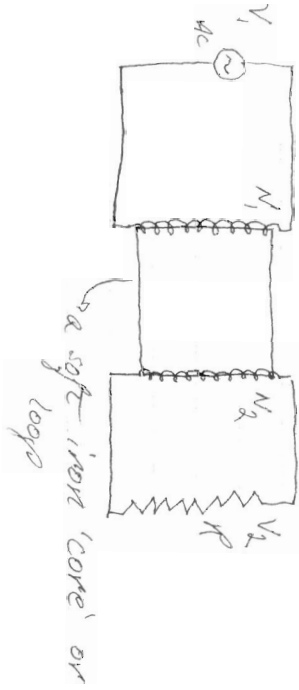
$$= 5 \times 10^{-5} \text{ F} \quad (= 50 \mu\text{F})$$

(3)

Transformers

(4)

- power distribution system
- want low voltage @ generation + end-user points
- want lowest possible current to reduce I^2R losses
- so need to have a voltage changing device: transformer



Coils:

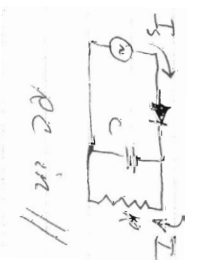
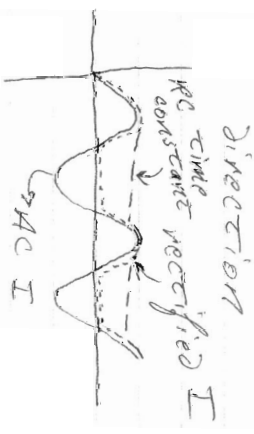
$$\left. \begin{aligned} V_1 &= -N_1 \frac{d\phi}{dt} \\ V_2 &= -N_2 \frac{d\phi}{dt} \end{aligned} \right\} V_2 = \frac{N_2}{N_1} V_1$$

if $N_2 > N_1$: "step up" transformer
 if $N_2 < N_1$: "step down" transformer
 current transformers: $i_1 V_1 = i_2 V_2$
 $i_1 = i_2 \left(\frac{N_1}{N_2} \right)$

Rectifier

(5)

- sometimes we want DC
- diodes allow current in one direction



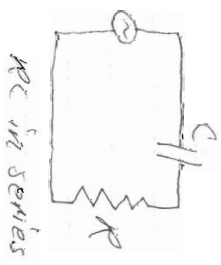
- when supplied I_s goes to 0, C discharges thru R & keeps I high
 - residual "ripple" undesirable

Filters

- recall $X_c = 1/\omega C$ is large when ω low

V_R - nonzero for high frequencies

V_C - nonzero for low frequencies



RC in series

