

# CH 3 HEAT, TEMP, ENTROPY

(i) mech into: have seen  
can make direct connection  
to ave'd gen. F's and W's  
therm. vels: can I find paroms  
which govern Q?

## HEAT FLOW

- WILL
- DEF. MACRO QTY'S TO DESCRIBE Q EXCHANGE
- ALL BASED ON PROB. (w/ FUND. POST.)

(ii) fine it dep. on  
micro details,  
we're not following,  
could imagine it's  
very complicated  
not wild  
find if  
look at  
sys. in  
equil, it  
dep. on  
only 1  
number,  
macroly  
accessible

will one system give E  
to another? yes, or no, if  
it's more likely; e, if there  
are many more ways for that  
to happen than not



ISOLATED: TOTAL  $E^{(0)} = E + E'$  CONST

INSULATED: E, E' CONST

⇒ MACRO CONSTRAINTS:  $E^{(0)}, E$  (Then  $E' = E^{(0)} - E$ )  
(choose these rather than E & E' since  $E^{(0)}$  will remain a const.)

KEEP ALL  $X_\alpha$  FIXED (NO W)

⇒ ALL SYS IN ENS. SATISFY THESE

IN EQUIL: ALL POSS. STATES EQ. LIKELY

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NOW:

REMOVE INSUL:

- RELAXES CONSTRAINT:

$E^{(0)}$  CONST., BUT E ( $\{E'\}$ ) CHG

-  $\Omega_f \geq \Omega_i$ : } # MICRO STATES POSSIBLE { by defn of constraint }  
HAVE

- ALL ORIGINAL STATES + (USUALLY MANY) MORE  
w/ DIFF. E, E'

-(MANY) NEW STATES APPEAR IN ENS.  
(assume big enough that all still well-represented)

IMMEDIATELY

- NOT IN EQUIL (USUALLY):

Q FLOWS UNTIL ALL  $P_T = \text{CONST}$   $\Rightarrow$  NEW EQUIL;  
 IN ENS:  $E(\frac{1}{2}E)$  WILL DIFFER

*\*\* emphasize: can't use fund post. during process unless do it QS; have to study at micro level in genl*

- CAN'T UNDO BY PUTTING INSUL. BACK IN  
 (would need to do more  $\rightarrow$  work on system)  
 (won't get heat to flow back)

10/18/02  
 (7)

example of

IRREVERSIBLE PROCESS:

- ISOLATED SYS.
- RELAX CONSTRAINT:

say { ANYTHING RESTRICTING STATES IN ENS.  
 (REIF:  $y \propto$  - MORE GENERAL THAN  $x \propto$ )

ex:  $E, N, V, \bar{p}, \dots$

anything known or set which can be used to exclude states from ens.

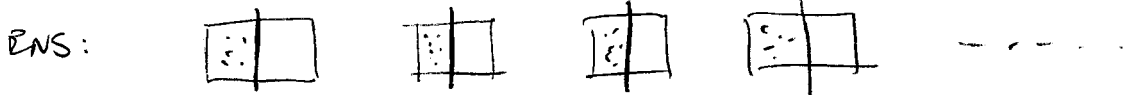
$\Rightarrow \Omega_f > \Omega_i$

$\Rightarrow$  CAN'T UNDO BY SIMPLY REVERSING ACTION  
 (ex put back wall, insulation)

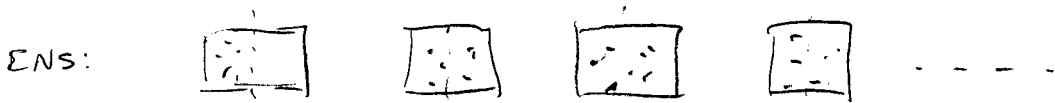
$\downarrow$  say  
 (already covered in intro)

ex PARTICLES IN BOX:

CONSTR: ALL ON LEFT VIA WALL



RELAX: REMOVE WALL



SMALL  
 SUBSET

$$\Omega_f \gg \Omega_i$$

HOW MUCH? (twice? not even close)

IN EQUIL:  $P(\text{ALL LEFT}) \text{ NOW} = \frac{1}{2^N} \quad N \sim 10^{24}$

FROM:  $P(\text{LEFT}) = \frac{\Omega_i}{\Omega_f} = \frac{1}{2^N} \sim \frac{1}{2^{10^{24}}}$

FUND. POST

(we only needed to pay atten to location, since  $\vec{p}$  played no role)

⇒ INITIAL CONFIGS SWAMPED BY NEW CONFIGS

⇒ VERY UNLIKELY TO FIND IN ORIG. <sup>CONFIG</sup> AFTER NEW EQUIL

- CAN'T UNDO BY PUTTING WALL BACK

(like Pandora's box; doesn't restore orig. configs in ens.)

- CAN IF INTERACT W/ ANOTHER SYS (but then not isolated)  
DOES WORK

### REVERSIBLE PROCESS

- RARE

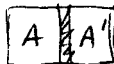
- RELAX ⇒  $\Omega_f = \Omega_i$  (ie doesn't gain access to new state)

⇒ REALLY WASN'T A CONSTRAINT

- CAN RESTORE BY REIMPOSING  
(no additional work)

(dumb example:  
 $0 < E < E^{(0)}$ ;  
or putting wall out &  
in again)

BACK TO:



$$E^{(0)} = E + E'$$

ALL PROB. DEPENDS ON  $\Omega$  (IN EQUIL)

⇒ WHAT'S NEW  $\bar{E}$ ?

⇒ IS Q LIKELY?

copy  
↑

skip

BACK TO  $A \leftrightarrow A'$ : Find new  $\bar{E}$  via fund post.

3.4

NEW  $\bar{E}$ ,  $Q$  DETERMINED BY

$$\Omega(E^{(0)}, E)_{\text{TOTAL}} = \Omega(E) \Omega'(E')$$

(# STATES AVAIL AT VARIOUS  $E$ 's)  $\uparrow$   $E^{(0)} - E$

[ $\Omega_{\text{COMBINED}}$  might be a better choice]

BEHAVIOR:

FROM POST:

$$P(E) = \frac{\Omega(E^{(0)}, E)}{\sum_E \Omega_{\text{TOT}}(E)}$$

EXPECT:

-  $\Omega(E)$ ,  $\Omega'(E')$  GROW RAPIDLY w/  $E$ ,  $E'$

-  $\Omega_{\text{TOTAL}}$  SHARPLY PEAKED AT SOME  $E = \bar{E}$  (MAX):

$$\Omega_{\text{TOTAL}} = \Omega(E) \Omega'(E^{(0)} - E)$$

AS  $E$  INCR:

GROWS FAST

SHRINKS FAST

(and v.v.)

(SHRINKING SEES IN WHEN  $E$  IS SIGNIFICANT FRACTION OF  $E^{(0)}$ )

(falls to zero when  $E \geq E^{(0)}$ )

FROM OUR EST:

$$\Omega(E) \sim E^f \quad \Omega'(E') \sim (E')^{f'}$$

$$\Omega_{\text{TOTAL}} \sim E^f (E^{(0)} - E)^{f'}$$

$\Rightarrow$  SHARP PEAK FOR  $f \sim 10^{24}$

EX

HW PROB:

$$\text{LET } f = f'$$

$$x \equiv$$

$$\frac{E}{E^{(0)}}$$

(fraction of  $E_{\text{TOTAL}}$  in sys A)

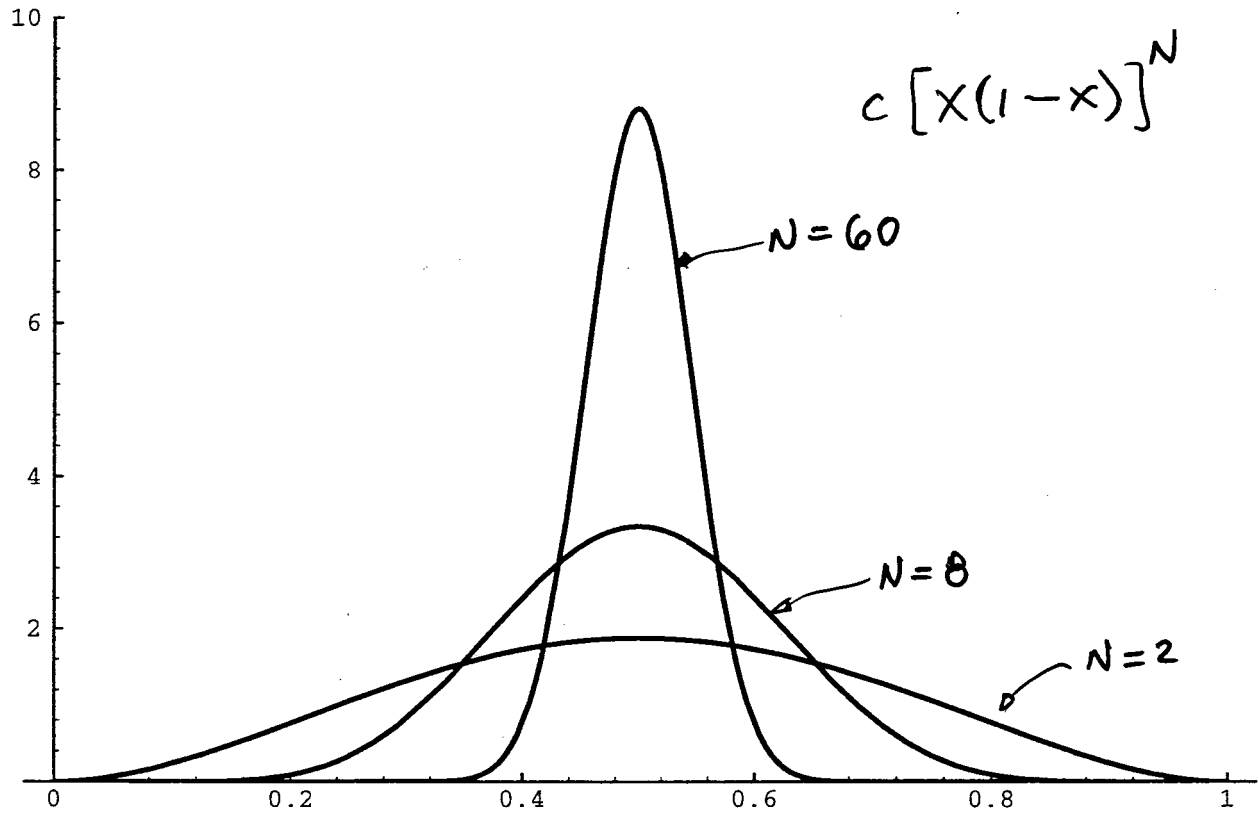
$$\Omega_{\text{TOT}} \sim E^{(0)2f} x^f (1-x)^f$$

SHARP PEAK NEAR  $x \sim \frac{1}{2}$  (cf PLOT)

imagine  $f = 10^{24}$

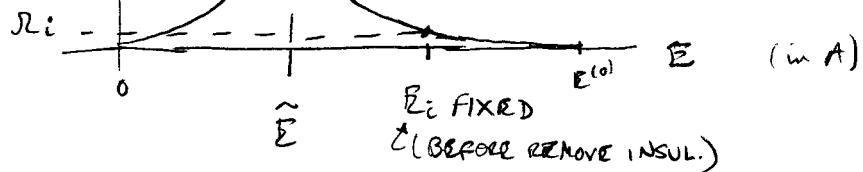
$\Rightarrow$  peak where dof share  $E$  equally: at peak

$$\frac{\partial \Omega_{\text{TOT}}}{\partial E} = 0 \Rightarrow \frac{E}{f} \approx \frac{E'}{f'}$$



IN GENERAL:

$$P(E) \propto \Omega_{TOT}(E^{(0)}, E) \\ = \Omega(E) \Omega'(E')$$



REMOVE INSUL:

- (1) MANY MORE STATES AVAIL, MOST NEAR  $\tilde{E}$  (i many more ways can have  $\tilde{E}$  than  $E_i$ )
- (2) MOST SYS. IN ENS. EXCHANGE ENERGY SO  $E \approx \tilde{E}$
- (3) NEW EQUIL

$$\bar{E} \approx \tilde{E} \Rightarrow \text{DETERMINES } Q \text{ (ave. of } E) \\ = \bar{E} - E_i$$

$E$  NOT FIXED, BUT LITTLE PROB TO FIND  $E \neq \bar{E} \approx \tilde{E}$

(so  $E$  near  $\tilde{E}$  is most important, since that's most probable, tho any  $E$  is possible up to  $E^{(0)}$ )

Start emphasizing: sharpness of distributions for macro systems is what makes stat mech useful

QTY'S ASSOCIATED w/ PEAK  $\tilde{E}$ : (i w/ new equil) (i what happens when bring together) (depends on 1 param)

$$P(E) = C \Omega_{TOTAL}(E^{(0)}, E) = C \Omega(E) \Omega'(E')$$

AT  $E = \tilde{E}$  P (OR  $\ln P$ ) IS MAX:

see later

[ WILL USE  $\ln \Rightarrow$  SMOOTHER FOR RAPIDLY INCR FNS  
 - CONVENIENT: TURNS  $\times$  TO  $+$   
 - MORE CLOSELY CONNECTED TO FAMILIAR QTY'S ]

$$\ln P = \ln C + \ln \Omega(E) + \ln \Omega'(E')$$

MAX

$$\frac{\partial \ln P}{\partial E} = \frac{\partial \ln \Omega(E)}{\partial E} + \frac{\partial \ln \Omega'(E')}{\partial E'} \frac{\partial E'}{\partial E} = 0$$

$\beta(E)$  (rate at which  $\ln(\#)$  states grows w/  $E$ )       $\beta'(E')$        $-1$

$(E' = E^{(0)} - E)$

$$\text{MAX} \Rightarrow \boxed{\beta(\tilde{E}) = \beta'(\tilde{E}') = \beta'(E^{(0)} - \tilde{E})}$$

AT MAX: rate at which number states gained by  $\Omega(E)$  = rate lost by  $\Omega'(E')$

23-10

DEFNS:

ABSOLUTE TEMP

DIMENSIONLESS

$$\left\{ kT \equiv \frac{1}{\beta} \right\} \text{dim} = \text{energy}$$

CONST w/ DIM OF ENERGY (depends on units)

SMALL T  $\leftrightarrow$  LARGE  $\beta \Rightarrow \Omega$  GROWS QUICKLY w/ E

LARGE T  $\leftrightarrow$  SMALL  $\beta$  " " SLOWLY "

$\Rightarrow \ln \Omega_{TOT}$  GROWS BY ENERGY E MORE. FROM <sup>SYS AT</sup> LARGE T TO SMALL T  
 (AS  $\tilde{E}$  MOVES TO  $\tilde{E}$ , Q FROM LARGE T TO SMALL UNTIL EQUAL)

note T is abstract  $\rightarrow$  can't look at a single microstate & pick out its T; macro qty; have in mind ...

ENTROPY

$$S \equiv k \ln \Omega$$

(DIM: ENERGY VIA  $k$ ; JUST A CONVENTION)

- $\ln$  OF AVAILABLE STATES
- MEAS OF HOW LIKELY TO FIND SYS W/ PARTIC. SET OF MACRO VALS: THAT CAN HAPPEN (from fund post)
- MEASURE OF RANDOMNESS OR DISORDER: (GIVES # WAYS)

⇒ LESS KNOWN ABOUT SYSTEM, MORE STATES AVAIL, LARGER  $S$  (ie FEWER CONSTR.)

⇒ "RANDOM" STATES ARE ELEMENTS OF SETS W/ MANY POSSIBILITIES (OF LICENSE PLATES)

THEN

$$\frac{1}{T} = \frac{\partial S}{\partial E}$$

(BY DEFN)

(lower  $T$ , more  $S$  incr. with  $E$ )

⇒  $P(E)$  IS MAX WHEN: (and so this is where most states are, determine  $\bar{E}$ )

(A)

$$E \equiv \bar{E}$$

$$\beta(\bar{E}) = \beta'(\bar{E}')$$

$$T = T'$$

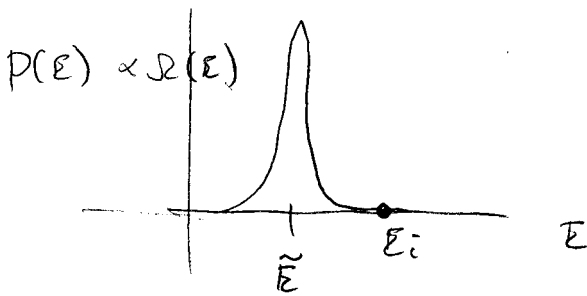
$$S + S' = \text{MAX}$$

additive

ALL PROPERTIES OF  $\Omega(E)$ ; NOTE THESE ARE STATISTICAL QTY'S BY DEFN. CAN'T LOOK INSIDE ONE SYS.  $\int$  SEE  $T$  OR  $S$  BY WATCH. PARTS; WOULDN'T DEF. FOR SMALL SYS. (note def.  $S$  as  $k \ln \Omega$  means add  $S$ 's) MULT  $\Omega$ 's → ADD  $S$ 's

SUMMARY (just say)

APPROACHING EQUIL:



skip drawing again?

AFTER REMOVE INSUL:

MOST AVAIL. STATES HAVE

$$E = \bar{E} \quad \therefore \text{IN EQUIL}$$

$$\bar{E} = \bar{E}$$

AS OCCUPY NEWLY ALLOWED STATES:

$$\bar{E}(t) \rightarrow \bar{E} = \bar{E}_+$$



OTHER PROPERTIES OF ABS TEMP T:

(1) SIGN       $\frac{1}{kT} \equiv \beta \equiv \frac{\partial \ln \Omega}{\partial E} > 0$

more E, more  $\Omega$

$$\boxed{T > 0}$$

(EXCEPTION: SPIN SYSTEM - <sup>artificial</sup> MOLECULES TIED DOWN (NO KE)  
HAS MAX E  $\rightarrow$  ALL ALLIGNED OP.  $\vec{B}$ )

AS APPROACH  $E_{MAX}$ ,  $\Omega$  DECREASES,  
( $T < 0$ )

(2) RELN TO E OF PARTICLES:

$$\Omega(E) \propto E^f$$

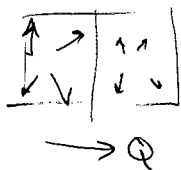
$$\ln \Omega \sim f \ln E + \text{const}$$

$$\beta \equiv \frac{\partial \ln \Omega}{\partial E} \sim \frac{f}{E} \Rightarrow \boxed{kT \approx \frac{E}{f}}$$

$$\Rightarrow \boxed{kT \sim \text{ENERGY PER DOF}} \quad (\text{very useful def.})$$

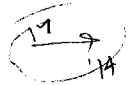
(familiar - high T, lots of E per molecule, etc)  
incl KE, INTERNAL E, ETC

slip  $\left\{ \Rightarrow \text{AS GO TO EQUIL}$



UNTIL ALL DOF HAVE  $\sim$  SAME E

(WE'VE SEEN IN COUNTING EXERCISES:  
RARE FOR FEW PARTICLES TO HAVE LOTS OF E)



3.7  
3.10

GAUSS APPROX FOR  $\Omega_{TOT}$  :

SHARPLY PEAKED - EXPAND  $\ln \Omega_{TOT}$  AT  $E = \tilde{E}$  :

$$\ln \Omega_{TOT}(E) = \ln[\Omega(E) \Omega'(E')] = \ln \Omega + \ln \Omega'$$

NEED

$$\begin{aligned} \frac{\partial \ln \Omega_{TOT}}{\partial E} &= \frac{\partial \ln \Omega}{\partial E} + \frac{\partial \ln \Omega'}{\partial E'} \underbrace{\left( \frac{\partial E'}{\partial E} \right)}_{-1} \\ & \qquad \qquad \qquad (E' = E^{(0)} - E) \\ &= \beta(E) - \beta'(E') \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 \ln \Omega_{TOT}}{\partial E^2} &= \frac{\partial^2 \ln \Omega}{\partial E^2} + \frac{\partial^2 \ln \Omega'}{\partial E'^2} \underbrace{\left( \frac{\partial E'}{\partial E} \right)^2}_{+1} \\ & \qquad \qquad \qquad \text{"} \qquad \qquad \qquad \text{"} \\ &= -(\lambda(E) + \lambda'(E')) \\ & \qquad \qquad \qquad \uparrow \\ & \qquad \qquad \qquad \text{since expect } < 0 \text{ at max} \end{aligned}$$

MAX :

$$\left. \frac{\partial \ln \Omega_{TOT}}{\partial E} \right|_{E = \tilde{E}} = 0 \Rightarrow \beta(\tilde{E}) = \beta'(\tilde{E}')$$

$$\Rightarrow T = T' \quad \text{WHEN} \quad E = \tilde{E} = \tilde{E}'$$

(KNOW THIS: same T at max)

$$\Rightarrow \ln \Omega_{TOT}(E) \sim \ln \Omega_{TOT}(\tilde{E}) - \frac{1}{2} (\underbrace{\lambda(\tilde{E}) + \lambda'(\tilde{E}')}_{\equiv \lambda_0}) (E - \tilde{E})^2 + \dots$$

$\Rightarrow \lambda_0 > 0$  IF AT MAX (if not max at equal T, wouldn't be at equil; would run away)

$\Rightarrow \lambda(\bar{E}) \} \lambda'(\bar{E}') \text{ BOTH } > 0$

(IF for ex  $\lambda(\bar{E}) < 0$ , could put two of these ident. sys. together  $\Rightarrow \lambda_0 = 2\lambda(\bar{E}) < 0$ ) (think what happens if  $p \sim \sqrt{V}$ )

$\Rightarrow \Omega_{TOT}(E) \approx \Omega_{TOT}(\bar{E}) e^{-\frac{1}{2} \lambda_0 (E - \bar{E})^2}$

$P(E) \propto \Omega_{TOT}(E)$  (FUND POST)

$\Rightarrow$  one sys gets all the E  
 $\Rightarrow$  sloshes around  
 $\Rightarrow$  wildly diff T's

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24

$\Rightarrow P(E) = P(\bar{E}) e^{-\frac{1}{2} \lambda_0 (E - \bar{E})^2}$

GAUSSIAN:

$\bar{E} = \bar{E}$  (exact in this approx)

$\sigma = \Delta^* E = \frac{1}{\sqrt{\lambda_0}}$  all determined by  $\Omega$

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How SHARP?

$\Omega(E) \sim E^f \quad \ln \Omega \sim f \ln E$

$-\lambda(E) = \frac{\partial^2 \ln \Omega}{\partial E^2} \sim -\frac{f}{E^2}$

AT  $\bar{E} = \bar{E}$ :  $\lambda_0 \sim +\frac{f}{\bar{E}^2}$  } taking  $f \approx f'$   
 $\lambda \approx \lambda'$

$\Rightarrow \frac{\Delta^* E}{\bar{E}} \sim \frac{1}{\sqrt{f}} \sim 10^{-12}$

VERY SHARP:

$P(E) \sim 0$  IF  $|\Delta E| \gtrsim 10^{-12} \bar{E}$

$\Rightarrow$  E FLUCTS, BUT RARE THAT MEAS. FLUCTUATION OF 1 PART/TRILLION  
 $\Rightarrow$  MOST MEAS. NOT PRECISE ENOUGH TO DETECT

SURPRISE: LARGER  $\dagger$

- $\Rightarrow$  MORE COMPLICATED SYS
- $\Rightarrow$  MORE PREDICTIVE  $P(E)$  BECOMES
- $\Rightarrow$  SIMPLICITY IN LARGE  $\#$ 'S

CONSEQUENCES OF SHARP PEAK / SMALL  $\Delta^*E$ :

(0) GAUSS APPROX  $\sim$  EXACT:  $\bar{E} = \hat{E}$   $\bar{E}' = E^{(0)} - \bar{E}$

(a) FLUCTS. ARE TINY  $\Rightarrow$  FEW SYS IN ENS HAVE  $E$  FAR FROM  $\bar{E}$   
 $\Rightarrow E$  STAYS CLOSE TO  $\bar{E}$  VS  $t$  FOR 1 SYS

(b) SIMILAR TO CASE WHERE  $E$  IS NOW EXACTLY  $\bar{E}$   
 $E'$  " "  $E^{(0)} - \bar{E}$

AND SEPARATELY ISOLATED

(c) IF  $\Delta^*E < 8E$  (ABILITY TO MEAS.) THEN IDENTICAL TO "

(d) BY OUR DEFN,  $T(\bar{E})$  NOT STRICTLY THE TEMP FOR A AFTER CONTACT w/ A'  
 $\Rightarrow T$  DEFINED FOR SYS AT DEFINITE  $E$  (w/IN  $8E$ )  
 $\Rightarrow A$  CAN HAVE  $0 < E < E^{(0)}$

BUT CAN IF (b)  $\&$  (c) TRUE

(NOTE:  $T$  NOT USEFUL FOR SMALL SYS w/ WIDE RANGE IN  $E$ 'S  
 $\Rightarrow$  HAS WIDE RANGE OF VALUES)

SINGLE SYSTEM:

(e)  $Q, T$  DEF'D VIA  $JL$  FOR ENS., NOT 1 SYS  $\Rightarrow$  GIVE AVES  
 IF NARROW: KNOW (w/ REL ERR  $10^{-12}$ )  
 $E_f = \bar{E}$   $\Delta E = \bar{E} - E_i = Q$  FOR SINGLE SYS

WHAT MAKES STATMECH USEFUL :

USUALLY STUDYING 1 SYS  $\equiv$  SYS IN MY LAB

- ONLY MEAS FEW MACRO PROPERTIES
- WOULD LIKE TO MAKE PREDICTIONS

IN PRINCIPLE

- MANY MICRO POSSIBILITIES CONSIST. w/ FEW KNOWN MACRO PROPS
- MUST CONSIDER SETS / ENSEMBLES
- ALL QTY'S PREDICTED ARE RELATED TO PROB. DISTR (AVES, # STATES, ...)
- ex  $Q, \beta, T, \bar{E}, S$  ...

$\Rightarrow$  GIVE PREDICTIONS FOR ENS.

$\Rightarrow$  GIVES RANGE OF " " MY 1 SYS

MACRO SYS

- DISTR. ARE NARROW FOR LARGE  $f$

$\Rightarrow$  CAN MAKE PRECISE PREDICTION FOR 1 SYS

ex HEAT EXCH: NEW  $\bar{E}$  w/  $\Delta^*E \sim 10^{-12} \bar{E}$

$\Rightarrow$  IN ENS. ALMOST ALL SYS HAVE  $E = \bar{E} \pm \underbrace{\Delta^*E}_{10^{-12} \bar{E}}$

$\Rightarrow$  MY SYS WILL HAVE  $E = \bar{E} \pm \Delta^*E$   
(i.e. ALMOST EXACTLY  $\bar{E}$ )

$\Rightarrow$  EXTREMELY UNLIKELY TO BE OFF BY  $10 \Delta^*E$

- MUST LOOK VERY HARD TO SEE FLUCTS;  
OFTEN TOO SMALL VS EXPTL ERROR

$\Rightarrow$  CAN MAKE VERY PRECISE PREDICTIONS FOR 1 SYS

(f) IN THIS SPIRIT (ie CAN TALK ABOUT SINGLE T EVEN AFTER Q) :

3.11.4

## 0<sup>TH</sup> LAW OF THERMO

- ORIGINALLY FROM OBSERVATION:

IF	SYS A	IN THERM EQ. W/	SYS C
AND	" B	" "	" C
THEN	" A	" "	" B

ie  $Q=0$

WHY? WE SHOWED THERM EQ. REQUIRES SAME  $\beta$ 'S (OR T'S)

$\Rightarrow$  IF  $\beta_A = \beta_C$  AND  $\beta_B = \beta_C$  THEN  $\beta_A = \beta_B$

$\Rightarrow$  SIMPLE PROPERTY OF REAL #'S

CONTENT: THERMAL EQUIL. DEP. ON SINGLE PARAMETER

SEEMS OBVIOUS?

SUPPOSE: DON'T KNOW ABOUT  $JR$

" " WHAT  $Q$  IS (A FLUID?)

IF KNEW

(1) NO  $Q$  FOR GLASS OF H<sub>2</sub>O IN CONTACT W/ ELEPHANT

(2) " SAME " " TOASTER

IS IT OBVIOUS NOTHING HAPPENS FOR TOASTER  $\leftrightarrow$  ELEPHANT?

3.11.4

(g) SIMPLIFIES PROPERTIES OF ENTROPY S:

(1) SE (ACC. OF MEAS.) DOESN'T MATTER MUCH:

(a)  $\Omega(E) = \omega(E) SE$  (ie  $\Omega \propto SE$ )

{ know for now  
 $SE \propto \Omega \times SE$   
 (cf.  $\omega$ )

$\ln \Omega = \ln \omega + \ln SE$

$\beta = \frac{\partial \ln \Omega}{\partial E} = \frac{\partial \ln \omega}{\partial E}$

$\Rightarrow \beta$  OR  $T$  INDEP OF  $SE$

all statistical props follow from  $\Omega$ ; seems arbitrary if it dps on my experimental abilities

(b)  $S = k \ln \Omega$

DIFF CHOICE FOR  $SE$ :  $SE \rightarrow SE^*$

$\Omega^* = \omega(E) SE^* = \Omega \cdot \left(\frac{SE^*}{SE}\right)$

$S^* = k \ln \Omega^* = k \left[ \ln \Omega + \ln \left(\frac{SE^*}{SE}\right) \right]$

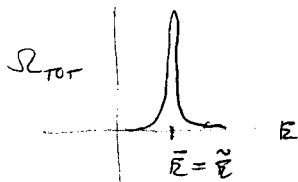
- f      ~ 1      even if  $SE^*$  differs by factor of 100

$\therefore S^* = S$

Stat mech: Hypothesis matters, not factors

(2) TWO SYSTEMS: <sup>can show</sup>  $S_{ALL E} \approx S(\bar{E}) + S'(\bar{E}')$  A A'

(ie same as if isolated again)



- ANY E POSSIBLE

$S_{A,E} = k \ln \Omega_{AE}^{TOT}$

$\Omega_{AE} = \int_0^{\dots} dE' \omega_{TOT}(E^{(0)}, E')$

$\frac{\Omega_{TOT}(E^{(0)}, E)}{SE}$

NARROW:

$$\int dE \Omega_{TOT}(E^{(0)}, E) \approx \Omega_{TOT}(E^{(0)}, \bar{E}) \Delta^* E \quad (\text{like } \delta \text{ for})$$

$$\Rightarrow S_{AE} \sim \Omega_{TOT}(E^{(0)}, \bar{E}) \left( \frac{\Delta^* E}{\delta E} \right)$$

SO

$$S_{AE} \sim \underbrace{k \ln \Omega_{TOT}(\bar{E})}_{\sim f} + \underbrace{k \ln \left( \frac{\Delta^* E}{\delta E} \right)}_{\sim 1} \rightarrow \text{NEGLECTIBLE}$$

$$k \ln \Omega(\bar{E}) + k \ln \Omega(\bar{E}')$$

$$= S(\bar{E}) + S'(\bar{E}') \quad (\bar{E} = \tilde{E} \quad \bar{E}' = E^{(0)} - \bar{E})$$

(this is example of statement that almost same as if system were locked exactly at  $E = \bar{E} = \tilde{E}$ )

$\Rightarrow$  We saw this in problem 2.4: spin- $\frac{1}{2}$  system

$$\ln \Omega(E=0) \approx N \ln 2 \Rightarrow \Omega \sim 2^N = \text{total \# possible for all spin configs}$$

$\frac{1}{2}$  up  $\frac{1}{2}$  dn

\* also note (if don't discuss (a)), that when compute  $S = k \ln \Omega$ , value of  $\delta E$  is irrelevant (again, cf. prob 2.4)

$$\ln \Omega = \underbrace{\ln \omega}_{\sim f} + \underbrace{\ln \delta E}_{\sim 1}$$



GEN'L INTERACTIONS:

ALLOW BOTH  $E$  &  $x$  TO CHANGE

1X PUT GASES IN CONTACT; AFTER EQUIL, WHERE'S WALL?



CP  $E$  TRANSFER:  $Q$  FLOWS UNTIL MOST SYS. IN ENS. NEAR  $\bar{E}$  WHERE  $\Omega$  (OR  $S$ ) IS MAX

HERE: HOW WILL WALL MOVE TO MAX  $\Omega$ ?

CP THERM INTS

- NEEDED TO KNOW HOW  $\Omega$  CHGD W/  $E$
- EQUIL. WHEN RATE SAME  $\Rightarrow T = T'$

NOW

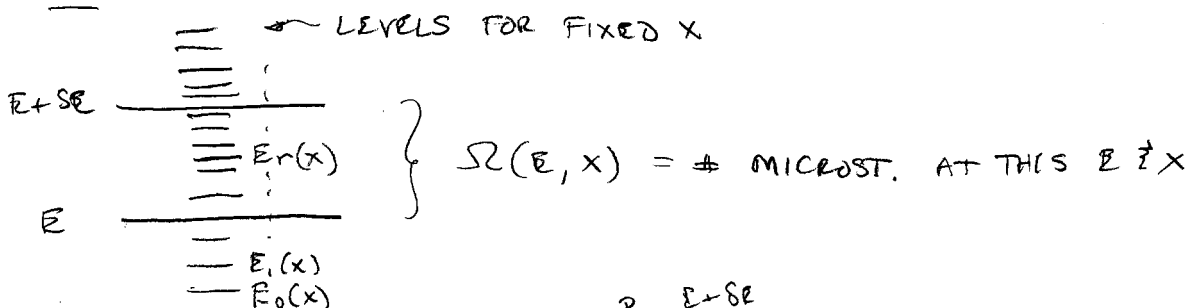
- NEED TO KNOW HOW  $\Omega$  CHGS W/  $x$

1B  
1A

ASSUME 1  $x$  FOR NOW

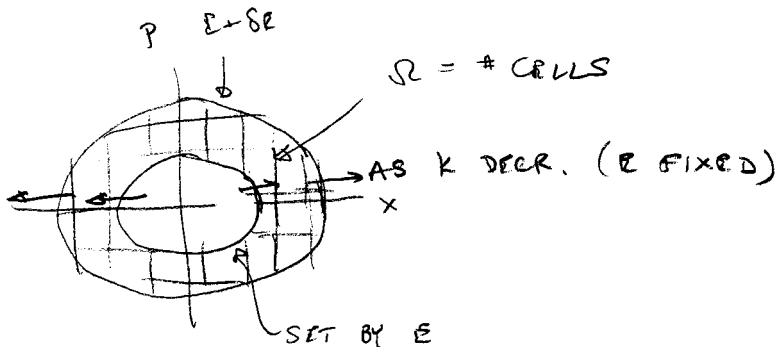
QM:  $E_r$  LEVELS ARE FNS OF  $x$

possible energy levels for entire sys



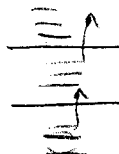
CLASSICAL (or HARM OSC)

w/ SPRING CONST = EXT PARAM



(WILL USE QM CASE)

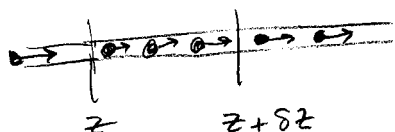
CHG  $x$ :  $E_r(x)$  CHG DIFF'LY  
 - SOME INSIDE LEAVE  
 - " OUTSIDE ENTER



$\Rightarrow$  WANT NET CHG IN  $\Omega = \#$  INSIDE

COMMON ANALOGOUS PROBLEM: PARTICLE (OR FLUID) FLOW  
- EASIER TO PICTURE

1D:

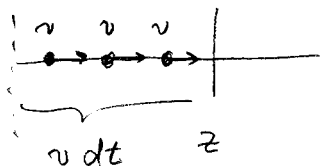


CALC CHG. IN DENSITY  $\rho(z) \equiv \frac{N_{\text{INSIDE}}}{\delta z}$  AS FLOWS

TO GET RATE  $\frac{d\rho}{dt} = \frac{dN_{\text{INS}}}{dt} \frac{1}{\delta z}$

1ST: CONSIDER RATE CROSS 1 PT.

2ND: COUNT (RATE IN) - (RATE OUT) AT  $z$  &  $z + \delta z$



(1) IF ALL HAVE VEL  $v$  w/ UNIFORM DENS

RATE CROSS  $z$

IN TIME  $dt$ , ALL IN LENGTH  $v dt$  CROSS

$$\Rightarrow dN = \# \text{ CROSSING} = \left( \frac{\# \text{ PARTS.}}{\text{LENGTH}} \right) \cdot \text{LENGTH} = \rho v dt$$

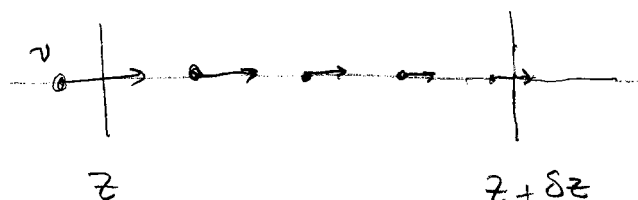
$\frac{1}{\delta z}$  ie CHG IN # ON PHS

$$\Rightarrow \text{RATE } \frac{dN}{dt} = \rho v = \frac{\# \text{ CROSS}}{\text{TIME}} \equiv \text{FLUX}$$

(SAME AT ALL  $z$  SO FAR)

(2) NOW ALLOW  $\rho$  TO DEP ON  $v$  &  $z$

$$\rho_v(z) \equiv \frac{\# \text{ PARTS. w/ VEL } v \text{ AT } z}{\text{LENGTH}}$$



} CAN HAVE PARTS.  
BUILD UP

ENTERING FROM LEFT IN  $dt$ :

(a) w/ VEL  $v$ :  $\rho_v(z) v dt$

(b) w/ ALL  $v$ 's:  $\sum_v \rho_v(z) v dt$

could also  
be Solv

LEAVING RIGHT:

$$\sum_v \rho_v(z + \delta z) v dt$$

CHG. INSIDE IN  $dt = \# \text{ ENTER} - \# \text{ LEAVE}$

$$dN_{\text{INS}} = \left[ \sum_v \rho_v(z) v - \sum_v \rho_v(z + \delta z) v \right] dt$$

(3) CAN SEE  $\rho$  WILL ALSO DEP. ON  $t \Rightarrow$  INCL AS VAR,

$$\frac{dN_{\text{INS}}}{dt} = \left[ \sum_v \rho_v(z, t) v - \sum_v \rho_v(z + \delta z, t) v \right]$$

BACK TO OUR PROBLEM: DICTIONARY

PARTICLE LABEL  $\rightarrow v$

$z \rightarrow E_r$

$t \rightarrow X$

$N_{\text{INS}}(z, t) \rightarrow \Omega(E, X)$

$v = \frac{dz}{dt} \rightarrow \frac{\partial E_r}{\partial X} \equiv -X_r$  GEN FORCE  
(ASSOC w/  $r$ )

LET  $\Omega_X(E, X) \equiv \# \text{ STATES w/ } \left. \begin{array}{l} E \text{ TO } E + \delta E \\ X \text{ TO } X + \delta X \end{array} \right\} \text{ie ORGANIZE STATES ACC. TO } X \text{ VALUES}$

$\rho_v(z, t) \rightarrow \frac{\Omega_X(E, X)}{\delta E} \equiv \omega_X(E, X) \left. \vphantom{\frac{\Omega_X(E, X)}{\delta E}} \right\} \text{DENS. OF STATES}$

18-17  
110-25  
12

THEN

$$\frac{dN_{ins}}{dt} \rightarrow \frac{\partial \Omega(E, x)}{\partial x} = \sum_X \left[ \frac{\Omega_X(E, x)}{\delta E} (-X) - \frac{\Omega_X(E + \delta E, x)}{\delta E} (-X) \right]$$

ENTER BOT. LEAVE TOP

ASSUME QUASI-STATIC (USE FUND POST)

$$\bar{X}(E, x) = \frac{\sum_X \Omega_X(E, x) X}{\Omega(E, x)}$$

PROB OF X  
HAVING PARTIC. VALUE  
∝ # STATES w/ "

$$\begin{aligned} \Rightarrow \frac{\partial \Omega(E, x)}{\partial x} &= \left[ -\Omega(E, x) \bar{X}(E, x) + \Omega(E + \delta E, x) \bar{X}(E + \delta E, x) \right] \frac{1}{\delta E} \\ &\sim \frac{\partial (E \bar{X})}{\partial E} \quad \text{IF } \delta E \ll E \\ &= \frac{\partial \Omega}{\partial E} \bar{X} + \Omega \frac{\partial \bar{X}}{\partial E} \end{aligned}$$

USING  $\ln \Omega$  :

$$\begin{aligned} \frac{\partial \ln \Omega}{\partial E} &= \frac{1}{\Omega} \frac{\partial \Omega}{\partial E} \\ \frac{\partial \ln \Omega}{\partial x} &= \frac{1}{\Omega} \frac{\partial \Omega}{\partial x} \end{aligned} \quad \left. \vphantom{\frac{\partial \ln \Omega}{\partial E}} \right\} \begin{array}{l} \text{REPLACE ABOVE} \\ \text{w/ LHS} \end{array}$$

$$\Omega \frac{\partial \ln \Omega}{\partial X} = \Omega \underbrace{\frac{\partial \ln \Omega}{\partial E}}_{\equiv \beta} \bar{X} + \Omega \frac{\partial \bar{X}}{\partial E}$$

$$\boxed{\frac{\partial \ln \Omega}{\partial X} = \beta \bar{X} + \frac{\partial \bar{X}}{\partial E}}$$

TYPICAL MACRO SYSTEM:

$$\Omega \sim e^f \quad \beta \bar{X} \sim \frac{f}{E} \bar{X} \quad \Rightarrow \quad \frac{\partial \bar{X}}{\partial E} \sim \frac{\bar{X}}{E}$$

MAIN RESULT FOR CH 3: (REPEAT EACH  $\alpha$ )

$$\Rightarrow \boxed{\frac{\partial \ln \Omega(E, x_\alpha)}{\partial x_\alpha} = \beta \bar{X}_\alpha(E, x_\alpha)}$$

Q-5

IN GENERAL, COULD REPEAT EACH OF SEVERAL EXT. PARAMS

ROUGH EST FOR ORDER OF MAGN. (FOR WANT OF ADDITIONAL INFO

ex  $f(x) = x^3$

$$\left( \frac{\partial f}{\partial x} = 3x^2 \quad \text{vs} \quad \frac{f}{x} = x^2 \right)$$

NOT BAD

OP TO

$$\boxed{\frac{\partial \ln \Omega}{\partial E} \equiv \beta}$$

(roughly like chain rule:  $\frac{\partial \ln \Omega}{\partial X} \sim \frac{\partial \ln \Omega}{\partial E} \frac{\partial E}{\partial X}$ )

NOTE: CONNECT CHOS IN  $\ln \Omega$  W/ MEAS'BLE QTY:  $T \left\{ \bar{X} \right.$  (with  $\bar{p}$ )

say

(KNOW HOW  $\ln \Omega$  VARIES IN GEN'L. WILL USE TO GET GEN'L EQUIL CONDITIONS)

EX MONATOMIC IDEAL GAS (CLASSICAL)

(1)

3.16

- IF KNOW  $\Omega(E, X_\alpha)$  CAN GIVE AVE FOR ALL MACRO VARS (IN EQUIL)
- " " SOMETHING ABOUT  $\Omega$ , CAN OFTEN AT LEAST RELATE "

[mention that often  $E$  varies and have  $\bar{E}$  here instead, (ie don't worry about putting  $\bar{E}$  everywhere) but for macro sys., so many, it's almost same]

IDEAL GAS:

MOST USEFUL VARS:  $E, V, T, \bar{p}, S$ .

(all related to  $\Omega(E, V)$ )  
 (S is abstract but will see it's very useful; not really a property of a single sys., but for your sys. you can ask how big is the set its a member of, or how random it is)

HAVE

$$\beta = \frac{\partial \ln \Omega}{\partial E}$$

$$\bar{X}_\alpha = \frac{1}{\beta} \frac{\partial \ln \Omega}{\partial X_\alpha}$$

$$\bar{p} = \frac{1}{\beta} \frac{\partial \ln \Omega}{\partial V}$$

KNOW (since ignoring forces between)

(1) # STATES AVAIL. FOR EACH MOL.  $\propto V$  (OBVIOUS)

$$\Omega = V^N \chi(E)$$

$E \sim \text{CHI}$

equiv. to each mol. equally likely anywhere from fund. post. (we actually know more)

THEN

$$\ln \Omega = N \ln V + \ln \chi(E)$$

$$\Rightarrow \bar{p} = \frac{1}{\beta} \frac{N}{V} = \frac{NKT}{V}$$

recall:

$$\Omega_{IG} \propto \int_{SE} d^3x_1 \dots d^3x_N d^3p_1 \dots d^3p_N$$

$$\frac{1}{V^N} \chi(E)$$

$\bar{p} V = NKT$

EG.

IDEAL GAS LAW

How would this differ for diatomic IG?

OTHER VERSIONS:

IN DENSITY  $n = N/V \Rightarrow \bar{p} = nKT$

IN MOLES  $\nu \equiv N/N_A \Rightarrow \bar{p} V = \nu N_A K T = \nu R T$   
 $\equiv R$  (GAS CONST)

$\Rightarrow$  EQN OF STATE: RELATES MACRO VARS

skip (sharply peaked  $\rightarrow \bar{p}$  not very diff from  $p$  meas;  $10^{-12}$  or so makes sense to talk simply about pressure in "system")

ALSO

$$\beta = \frac{\partial \ln \Omega}{\partial E} = \frac{\partial \ln \chi(E)}{\partial E}$$

FN OF E ONLY

$$\Rightarrow T = T(E) \quad \text{OR} \quad \boxed{E = E(T)} \quad \text{IG}$$

CCP TO INTERACTING MOLES:  $E = E(T, V)$ SINCE SMALL  $V \rightarrow$  CLOSER TOGETHER  $\rightarrow$   $E$  DROPS (IF ATTRACTIVE)

CONTENT:  $\boxed{\Omega \propto V^N}$  FOR IG } like magic how much follows from so little input  
(for both relns)

(2) WE KNOW MORE ABOUT  $\Omega$ 

$$\Omega = B V^N E^{3N/2} \quad (\text{N LARGE; MONATOMIC IG})$$

↑  
CONST

$$\beta = \frac{\partial \ln \Omega}{\partial E} = \frac{\partial}{\partial E} \left( \frac{3N}{2} \ln E \right) = \frac{3}{2} \frac{N}{E}$$

$$\frac{1}{KT}$$

$$\Rightarrow \boxed{E = \frac{3}{2} NKT} \quad \text{MON IG}$$

(will see in HW that diatomic is slightly diff)

(RECALL EST:  $KT \sim E/f$  HERE  $f = 3N \Rightarrow \frac{E}{3N} = \frac{1}{2} KT \checkmark$ )

$\Rightarrow$  CAN GIVE ALL QTY'S, <sup>LISTED</sup> FOR MON IG IF KNOW  $E$  &  $V$ :

$$T = \frac{2}{3} \frac{1}{NK} E$$

$$\bar{p} = \frac{2}{3} \frac{E}{V} \quad \left. \begin{array}{l} \text{RECALL HW REIF 2.7} \\ \text{SAME FOR QM PART IN BOX} \end{array} \right\}$$

$$S = k \ln \Omega = k \left( N \ln V + \frac{3N}{2} \ln E \right) + \text{CONST}$$

{ WARNING:

- ASSUME HERE  $E$  KNOWN (w/in SE)  $\Rightarrow$   $T$  HAS SINGLE VALUE (for ex)

- ONCE SYS IN THERMAL CONTACT, TAKES RANGE OF VALUES

$\Rightarrow$  SHOULD USE  $\bar{E}$  (NOT  $E$ )

- MACRO SYS:  $P(E)$  SHARP (IN EQUIL)

$\Rightarrow$  KNOWING  $\bar{E} \sim$  SAME AS KNOWING  $E$

$\Rightarrow$  CAN REPLACE  $E$  w/  $\bar{E}$  IN ABOVE RELNS

} ONLY NEED TO DISTINGUISH WHEN PREDICT  $\Delta^* E$ , FOR EX