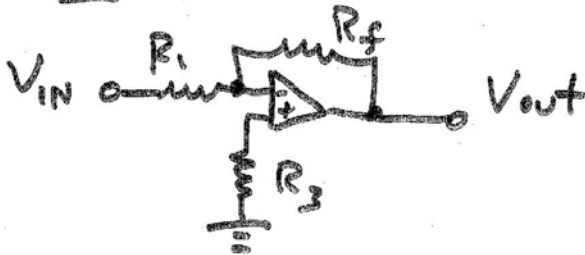


EX. 4.6 p. 210



①  $G = -100 = -R_f/R_1$ . CHOOSE  $R_1 = 10\text{ k}\Omega$   
 $R_f = 1\text{ M}\Omega$

② OTHER CHOICES OK.  
 INPUT BIAS CURRENT COMPENSATION:

SET  $R_3 = R_1 \parallel R_f$  (SEE LAB MANUAL  
 $\approx 10\text{ k}\Omega$  P. 141 ff.)

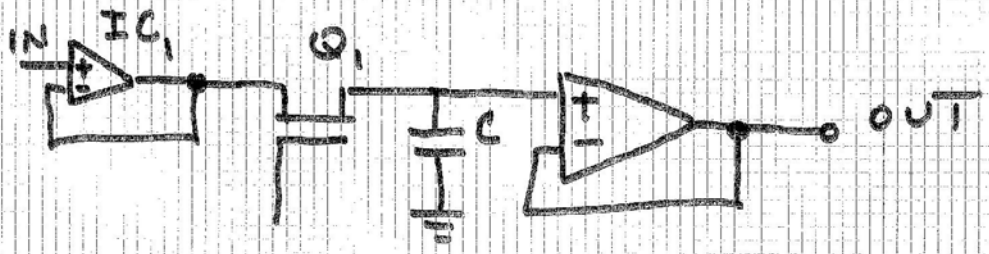
③ OFFSET TRIMMING:



④ HIGH  $Z_{IN}$ :



EX 4.8 P220



C CHARGES FROM I FROM  $I_{C1}$ , THIS CURRENT IS FINITE. CHARGING RATE OF C = SLEW RATE

$$\frac{dV}{dt} = \frac{I_{OUT}^{MAX}}{C} = 10^{-2} A / 0.01 \mu F$$

SLEW RATE = 1 V/ $\mu$ S SEE P27 ff.

EX 4.8, Q2.

OUTPUT OF IC<sub>1</sub> FOLLOWS INPUT  
AND SOURCES SOME I.

$$I_{IC_1}^{OUT} = C \left. \frac{dV}{dt} \right|_{IN}$$

$$= 0.01 \mu F \times 0.1 V/\mu S = 10^{-3} A.$$

THIS I PRODUCES VOLTAGE DROP  
ACROSS EFFECTIVE R<sub>E</sub> OF Q1.



VOLTAGE DROP ACROSS R:

$$V = IR$$

$$= 10^{-3} A \times 50 \Omega$$

$$V = 50 \text{ mV}$$

EX 4.8, P220, 03.

DROOP RATE ( $dV_c/dt$ ) IS JUST DUE  
TO CHARGE LEAKING OFF OF C.

$$I_{\text{LEAK}} = C \, dV/dt$$

$$\Rightarrow dV/dt = I_L/C = 1 \text{ nA} / .01 \mu\text{F}$$

$$\therefore \text{DROOP RATE} = 0.1 \text{ V/S}$$